## The Preparation of Ti<sub>5</sub>S<sub>8</sub>

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Ti<sub>5</sub>S<sub>8</sub> (12R type), which had never been prepared in a pure state, was obtained as a single phase by the chemical-transport method. The conditions for the preparation were determined experimentally. The existence range of the phase was examined for composition and temperature.

Several phases have been reported in the TiS-TiS<sub>2</sub> composition range, namely, TiS (2H),  $Ti_8S_9$  (9R),  $Ti_4S_5$  (10H),  $Ti_3S_4$  (21R),  $Ti_2S_3$  (4H),  $Ti_5S_8$  (12R), and TiS<sub>2</sub> (2H). (The designations in parenthesis indicate the structures in the Ramsdell notation.) Of these, the TiS phase is of the NiAs-type, while TiS2 is of the CdI2-type, structure. Both have a hexagonal close packed of sulfur. However, the intermediate phases have complex structures involving both the hexagonal and cubic packing of sulfur and varying stacking sequences, with a specific titanium-to-sulfur ratio. Titanium atoms are situated in the octahedral holes of the sulfur packing.

In spite of many reports on titanium sulfide, its phase diagram has not yet been established because of the variation in experimental data reported by many investigators, as has been pointed out by Jeannin<sup>1)</sup> or Kjekshus and Pearson.<sup>2)</sup> Furthermore, Tronc and Huber<sup>3)</sup> reported that, at the composition of Ti<sub>1.18</sub>S<sub>2</sub>, there are many structures with different periods in the c-direction, e.g., polytypism. These observations have indeed indicated that the titaniumsulfur system is complicated.

The existence of Ti<sub>5</sub>S<sub>8</sub> has been reported by Jeannin,4) Flink et al.,5) and Tronc and Huber,3) although it was not prepared by any of them as a single phase. They obtained it as a mixture with other structures, like Ti<sub>2</sub>S<sub>3</sub> (4H type). We ourselves were not able to prepare Ti<sub>5</sub>S<sub>8</sub> from the respective elements sealed in an evacuated silica tube. However, Ti<sub>5</sub>S<sub>8</sub> was obtained as a single phase by the chemicaltransport method when iodine was used as the transport agent. The aim of this paper is to describe the experimental conditions needed to obtain Ti<sub>5</sub>S<sub>8</sub> as a single phase.

The preparation conditions of Ti<sub>5</sub>S<sub>8</sub> will first be described, and then procedure for the identification of the obtained Ti<sub>5</sub>S<sub>8</sub>. Finally, the range of composition and temperature of Ti<sub>5</sub>S<sub>8</sub> will be shown.

## Results

Preparation Conditions. The preparation of Ti<sub>5</sub>S<sub>8</sub> was performed according to the following procedure. The titanium sulfide (1.5 g), the composition and structure of which will be described later, and the iodine (0.15 g) were sealed in an evacuated silica tube 150 mm in length and 12 mm inner diameter. The tube was held in a horizontal resistance furnace, where the high-temperature end was set at 600 °C and the low-temperature end at 500 °C. The titanium sulfide was transported from the low- to the high-temperature side. The transported titanium sulfide was then deposited as plate-shaped, grey-black crystals.

To prepare Ti<sub>5</sub>S<sub>8</sub> in a pure form by chemical transport, several important factors had to be ascertained: (1) the preparation temperature of the starting material, (2) the composition of the starting material, (3) the transport temperature, and (4) the iodine concentration. The specimen obtained by chemical transport was influenced by the following factors.

The Effect of the Preparation Temperature of the Starting The synthesis of the titanium sulfide used as the starting material was carried out according to the following procedure. Titanium metal powder (purity, 99.0%) and sulfur (purity, 99.9999%) were mixed together in a calculated ratio; the mixture was then allowed to react for a few days at 350 °C, after which the temperature was raised to 500-900 °C. With respect to the composition in the range from Ti<sub>1,38</sub>S<sub>2</sub> to Ti<sub>1,16</sub>S<sub>2</sub>, at 500 °C the structure of the specimen was of the 2H type; at 600-700 °C, a disordered stacking of the sulfur layers was detected, and above 800 °C the 4H type was the result. The 2H type specimen prepared at 500 °C might have been heterogeneous because of the incomplete reac-

By using the 2H type as the starting material, the transport was found to take place, but when the starting materials prepared at a temperatures above 600 °C were used, transport did not occur. The reason for this was not clear. However, it can be seen from Table 1 that whether or not the transport take place is dependent on the crystal structure of the starting material.

The Effect of the Composition of the Starting Material. How the transport was influenced by the composition of the starting material was then examined. The curve in Fig. 1 shows the transport rate versus the composition of the starting material. As can be seen

Table 1. Relation of the preparation temperature OF THE STARTING MATERIAL AND AVERAGE TRANSPORT RATE

Iodine concentration: 5.96 mg cm<sup>-3</sup>, transport time: 144 h, composition of the starting material: Ti<sub>1.21</sub>S<sub>2</sub>, temperature: 500 °C (low-temperature end) -> 600 °C (high-temperature end).

Temp/°C	Structure	Transport rate/mg h <sup>-1</sup>
500	TiS <sub>2</sub> (2H) type	0.8
600	Random	Negligibly small
700	Random	Negligibly small
800	$Ti_2S_3(4H)$ type	0
900	$Ti_2S_3(4H)$ type	0

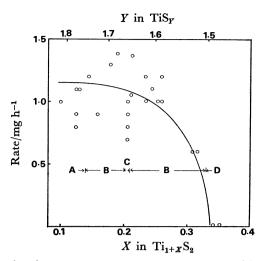


Fig. 1. Average transport rate versus composition of the starting material. (Iodine concentration: 5.96 mg cm<sup>-3</sup>, transport time: 144 h, temperature: 500 °C(low temperature side)→600 °C(high temperature side)).
A: Phase with disordered stacking of sulfur layers,
B: mixed phase of Ti<sub>2</sub>S<sub>3</sub> and Ti<sub>5</sub>S<sub>8</sub>, C: single phase of Ti<sub>5</sub>S<sub>8</sub>, D: no transport took place.

Table 2. Relation of the transport temperature and transported crystals

Iodine concentration: 5.96 mg cm<sup>-3</sup>, transport time: 144 h, composition of the starting material: Ti<sub>1.21</sub>S<sub>2</sub>.

Temp/°C	Transported crystal
400→500	
500→600	$\mathrm{Ti_{5}S_{8}}$
600→700	$\mathrm{Ti_5S_8} + \mathrm{Ti_2S_3}$
700→800	$\mathrm{Ti_5S_8} + \mathrm{Ti_2S_3}$

from this figure, the titanium sulfide was not transported by using a starting material whose composition was poorer in sulfur than  $\mathrm{Ti}_{1.33}\mathrm{S}_2$ . The transported crystals were composed of a mixed phase consisting of  $\mathrm{Ti}_2\mathrm{S}_3$  and  $\mathrm{Ti}_5\mathrm{S}_8$  when  $\mathrm{Ti}_{1.33}\mathrm{S}_2\mathrm{-Ti}_{1.22}\mathrm{S}_2$  was used as the starting material. A single phase of  $\mathrm{Ti}_5\mathrm{S}_8$  resulted when  $\mathrm{Ti}_{1.21}\mathrm{S}_2$  was used. A mixed phase of  $\mathrm{Ti}_2\mathrm{S}_3$  and  $\mathrm{Ti}_5\mathrm{S}_8$  resulted when  $\mathrm{Ti}_{1.19}\mathrm{S}_2\mathrm{-Ti}_{1.14}\mathrm{S}_2$  was used and a phase with disordered stacking of sulfur layers when a specimen richer in sulfur than  $\mathrm{Ti}_{1.13}\mathrm{S}_2$  was used.

Therefore, Ti<sub>5</sub>S<sub>8</sub> in a pure form was obtained by using a starting material whose composition was Ti<sub>1,21</sub>S<sub>2</sub>. The sulfur content of the transported crystals was always found to be smaller than that of the starting materials.

The Effect of the Transported Temperature. The transport was carried out at various temperatures in order to determine the most suitable temperature conditions. As can be seen in Table 2,  $\mathrm{Ti}_5\mathrm{S}_8$  was obtained in a pure form only at the temperature of 500 °C (low temperature side)  $\rightarrow 600$  °C (high temperature side). At any temperature above this, the transported crystals were found to be two phases consisting of  $\mathrm{Ti}_5\mathrm{S}_8$  and  $\mathrm{Ti}_2\mathrm{S}_3$ . From the observation of the electron diffractometry, it was found that the needleshaped crystal was  $\mathrm{Ti}_2\mathrm{S}_3$ , and the plate-shaped one,

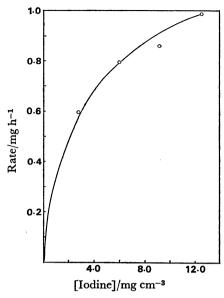


Fig. 2. Average transport rate versus iodine concentration. (Transport time: 144 h, composition of the starting material: Ti<sub>1.21</sub>S<sub>2</sub>, temperature: 500 °C (low temperature side)→600 °C (high temperature side)).

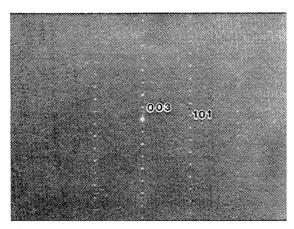


Fig. 3. Electron diffraction photograph of Ti<sub>5</sub>S<sub>8</sub> obtained by the chemical transport method.

Ti<sub>5</sub>S<sub>8</sub>.

On the contrary, the transport was found no longer to take place at temperature below 500 °C (low temperature end)—600 °C (high temperature end).

The Effect of the Iodine Concentration. In order to determine the most suitable conditions, the transport was carried out at various iodine concentrations. The results are shown in Fig. 2, where the transport rate increases with the increase in the iodine concentration. Crystals with stacking faults were produced at concentrations of more than 12 mg cm<sup>-3</sup>.

Identification by Means of Electron and X-Ray Diffractometry. Figure 3 shows an electron diffraction pattern taken from a crystal fragment obtained by grinding a transported crystal. The incident beam was directed parallel with the [010] direction. The distance of the repeating unit along the c-axis in the hexagonal setting was found to be  $34 \, \text{Å}$ , containing 12 layers. The systematic absence, -h+k+l=3n, in-

Table 3. Indices, calculated, and observed d-spaces and intensities

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
1       0       -2       2.928       2.929       21       2         0       0       12       2.857       *         1       0       4       2.808       2.811       16       1         1       0       -5       2.727       2.728       51       4         1       0       7       2.540       2.542       98       9         1       0       -8       2.442       2.443       62       6         1       0       10       2.245       2.246       100       10         1       0       11       2.150       2.151       9       1         1       0       13       1.972       1.973       7       7         0       0       18       1.903       1.904       3       *1         1       0       -14       1.889       1.889       54       5         1       0       16       1.737       1.737       19       1         1       1       0       1.716       1.717       87       *5         1       0       17       1.668       1.668       21       2
0       0       12       2.857       *         1       0       4       2.808       2.811       16       1         1       0       -5       2.727       2.728       51       4         1       0       7       2.540       2.542       98       9         1       0       -8       2.442       2.443       62       6         1       0       10       2.245       2.246       100       10         1       0       -11       2.150       2.151       9       1         1       0       13       1.972       1.973       7         0       0       18       1.903       1.904       3       *1         1       0       -14       1.889       1.889       54       5         1       0       16       1.737       1.737       19       1         1       0       17       1.668       1.668       21       2         1       1       6       1.643       1.639       10         1       0       19       1.541       1.541       6         1       0       2
1       0       4       2.808       2.811       16       1         1       0       -5       2.727       2.728       51       4         1       0       7       2.540       2.542       98       9         1       0       -8       2.442       2.443       62       6         1       0       10       2.245       2.246       100       10         1       0       -11       2.150       2.151       9       1         1       0       13       1.972       1.973       7       0         0       0       18       1.903       1.904       3       *1         1       0       -14       1.889       1.889       54       5         1       0       16       1.737       1.737       19       1         1       1       0       1.716       1.717       87       *5         1       0       17       1.668       1.668       21       2         1       1       6       1.643       1.639       10         1       0       19       1.541       1.541       6
1       0       -5       2.727       2.728       51       4         1       0       7       2.540       2.542       98       9         1       0       -8       2.442       2.443       62       6         1       0       10       2.245       2.246       100       10         1       0       -11       2.150       2.151       9       1         1       0       13       1.972       1.973       7         0       0       18       1.903       1.904       3       *1         1       0       -14       1.889       1.889       54       5         1       0       16       1.737       1.737       19       1         1       0       16       1.716       1.717       87       *5         1       0       17       1.668       1.668       21       2         1       1       6       1.643       1.639       10         1       0       19       1.541       1.541       6         1       0       20       1.484       4
1     0     7     2.540     2.542     98     9       1     0     -8     2.442     2.443     62     6       1     0     10     2.245     2.246     100     10       1     0     -11     2.150     2.151     9     1       1     0     13     1.972     1.973     7       0     0     18     1.903     1.904     3     *1       1     0     -14     1.889     1.889     54     5       1     0     16     1.737     1.737     19     1       1     1     0     1.716     1.717     87     *5       1     0     17     1.668     1.668     21     2       1     1     6     1.643     1.639     10       1     0     19     1.541     1.541     6       1     0     20     1.484     4
1     0     -8     2.442     2.443     62     6       1     0     10     2.245     2.246     100     10       1     0     -11     2.150     2.151     9     1       1     0     13     1.972     1.973     7       0     0     18     1.903     1.904     3     *1       1     0     -14     1.889     1.889     54     5       1     0     16     1.737     1.737     19     1       1     1     0     1.716     1.717     87     *5       1     0     17     1.668     1.668     21     2       1     1     6     1.643     1.639     10       1     0     19     1.541     1.541     6       1     0     20     1.484     4
1     0     10     2.245     2.246     100     10       1     0     -11     2.150     2.151     9     1       1     0     13     1.972     1.973     7       0     0     18     1.903     1.904     3     *1       1     0     -14     1.889     1.889     54     5       1     0     16     1.737     1.737     19     1       1     1     0     1.716     1.717     87     *5       1     0     17     1.668     1.668     21     2       1     1     6     1.643     1.639     10       1     0     19     1.541     1.541     6       1     0     20     1.484     4
1     0     -11     2.150     2.151     9     1       1     0     13     1.972     1.973     7       0     0     18     1.903     1.904     3     *1       1     0     -14     1.889     1.889     54     5       1     0     16     1.737     1.737     19     1       1     1     0     1.716     1.717     87     *5       1     0     17     1.668     1.668     21     2       1     1     6     1.643     1.639     10       1     0     19     1.541     1.541     6       1     0     20     1.484     4
1     0     13     1.972     1.973     7       0     0     18     1.903     1.904     3     *1       1     0     -14     1.889     1.889     54     5       1     0     16     1.737     1.737     19     1       1     1     0     1.716     1.717     87     *5       1     0     17     1.668     1.668     21     2       1     1     6     1.643     1.639     10       1     0     19     1.541     1.541     6       1     0     20     1.484     4
0     0     18     1.903     1.904     3     *1       1     0     -14     1.889     1.889     54     5       1     0     16     1.737     1.737     19     1       1     1     0     1.716     1.717     87     *5       1     0     17     1.668     1.668     21     2       1     1     6     1.643     1.639     10       1     0     19     1.541     1.541     6       1     0     20     1.484     4
1     0     -14     1.889     1.889     54     5       1     0     16     1.737     1.737     19     1       1     1     0     1.716     1.717     87     *5       1     0     17     1.668     1.668     21     2       1     1     6     1.643     1.639     10       1     0     19     1.541     1.541     6       1     0     20     1.484     4
1     0     16     1.737     1.737     19     1       1     1     0     1.716     1.717     87     *5       1     0     17     1.668     1.668     21     2       1     1     6     1.643     1.639     10       1     0     19     1.541     1.541     6       1     0     20     1.484     4
1 1 0 1.716 1.717 87 *5 1 0 17 1.668 1.668 21 2 1 1 6 1.643 1.639 10 1 0 19 1.541 1.541 6 1 0 20 1.484 4
1 0 17 1.668 1.668 21 2 1 1 6 1.643 1.639 10 1 0 19 1.541 1.541 6 1 0 20 1.484 4
1 1 6 1.643 1.639 10 1 0 19 1.541 1.541 6 1 0 20 1.484 4
1 0 19 1.541 1.541 6 1 0 20 1.484 4
1 0 20 1.484 4
1 0 20 10111
0 0 9 1 491
2 0 2 1.481
$2  0  -4  1.464 \qquad 2$
2 0 5 1.452 5
0 0 24 1.427 1.428 14 *6
$2  0  -7 \qquad 1.422  1.418 \qquad 12$
2 0 8 1.404 1.403 8
1 0 22 1.379 2
2 0 -10 1.363 1.363 15 2
2 0 11 1.341 2
$2  0  -13 \qquad 1.244 \qquad \qquad 1$
1 1 18 1.274 1.274 4
2 0 14 1.270 1.270 11

\* Indicates the indices affected by the preferred orientation.

dicates the rhombohedral symmetry of the structure. Therefore, the structure of this crystal may be referred to as a 12R type using Ramsdell notation, this is consistent with the structure of  ${\rm Ti}_5{\rm S}_8$  as described by Flink *et al.*, 5 and Tronc and Huber. 3

The powder X-ray diffraction pattern of the Ti<sub>5</sub>S<sub>8</sub> sample (composition, Ti<sub>1.31</sub>S<sub>2</sub>) obtained by crushing the transported crystals was taken by the counterdiffractometer technique using Ni-filtered Cu Ka radiation. The pattern was indexed on the basis of the hexagonal cell (a=3.431 and c=34.25 Å), where the systematic absence,  $-h+k+l\neq 3n$ , is consistent with the case of the electron diffraction. Powder X-ray diffraction intensities were calculated for the structure model by Tronc et al.6) for the composition of Ti1.31S2 (Ti<sub>5</sub>S<sub>8</sub> phase) with an overall temperature factor of B=1.0. The intensities, calculated and observed, are listed in Table 3. These do not agree with each other for the 00l and 110 peaks because of the preferred orientation in the sample. The reliability factor R, defined by  $R=\sum |I_{obsd}-I_{calcd}|/\sum |I_{obsd}|$ , was 0.39; this was excessive. However, the R-value estimated by eliminating the 00l and 110 peaks, which were affected by the preferred orientation, was 0.14. There-

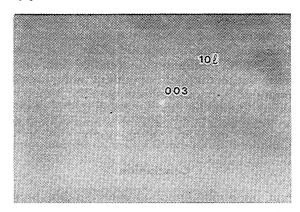


Fig. 4. Electron diffraction photograph of the specimen annealed at 1200 °C.

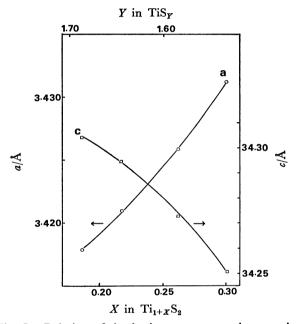


Fig. 5. Relation of the lattice constants and composition.

fore, this specimen was identified as Ti<sub>5</sub>S<sub>8</sub> (12R type), as has previously been reported by Tronc et al.<sup>6</sup>)

The information obtained from X-ray and electron diffractometry showed that the specimen prepared by the method described above was indeed a pure single phase and did not contain any other phases, like Ti<sub>2</sub>S<sub>3</sub> (4H type) or TiS<sub>2</sub> (2H type).

Range of the Temperature and Composition in Which The range of temperature and Ti<sub>5</sub>S<sub>8</sub> Can Exist. composition in which Ti<sub>5</sub>S<sub>8</sub> can exist was also examined. At first, Ti<sub>5</sub>S<sub>8</sub> (composition Ti<sub>1,23</sub>S<sub>2</sub>) was kept in evacuated tubes at 800, 900, 1000, 1100, and 1200 °C for 3 d. Disorder in sulfur stacking at 1100 °C and 1200 °C was found, although no change was detected in the specimens annealed below 1000 °C. Figure 4 is an electron-diffraction photograph of the specimen annealed at 1200 °C. In this figure, the diffusion for  $h-k=3n\pm 1$  shows disorder caused by sulfur stacking.<sup>7)</sup> At 1100 °C, Ti<sub>5</sub>S<sub>8</sub> began to change to another structure, but the rate of the transformation was so slow that a stable structure could not be ascertained at this temperature.

The composition range where the  ${\rm Ti}_5 S_8$  phase could exist was examined through the sulfurization or desulufurization in the atmosphere of the  ${\rm H_2-H_2S}$  mixture at 900 °C. After being quenched from 900 °C to room temperature, the specimens were examined by means of X-ray diffractometry. The lattice constants are shown in Fig. 5. From this experiment, it was found that  ${\rm Ti}_5 S_8$  can exist in compositions from at least  ${\rm Ti}_{1.31} S_2$  to  ${\rm Ti}_{1.16} S_2$  at 900 °C.

## Conclusion

From the results presented above, it can be concluded that: (1)  $\text{Ti}_5 S_8$  in a pure form can be prepared by the chemical transport method under the following conditions: transport agent; iodine (6—9 mg cm<sup>-3</sup>), starting material; titanium sulfide (composition  $\text{Ti}_{1.21} S_2$ ) prepared at 500 °C, transport temperature; 500 °C (low temperature end)  $\rightarrow$ 600 °C (high temperature end), and (2)  $\text{Ti}_5 S_8$  can exist over a large composition range at 900 °C.

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